



CO₂ Emissions from Heavy Duty Vehicles Overview of VECTO's inputs

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Outline

- Introduction
- Inputs & VECTO
 - Engine module (draft)
 - Transmission module (draft)
- Verification summary
- Conclusions – Follow up



INTRODUCTION



About the JRC / STU

- Joint Research Centre (JRC) research body of the European Commission
- Mission: provide research & innovation oriented to policy support for the European Union
- Sustainable transport unit: Research group working on transport technology & sustainability
- ~60 people, 7 labs, several models and software tools





Monitoring CO₂ from Heavy Duty Vehicles

- Need for an HDV CO₂ monitoring scheme for Europe
- Heavy Duty Vehicles is a complex sector, *"not 2 vehicles identical"*
- European manufacturers are amongst global leaders
- Lack of data to support policy, need for monitoring – data collection
- Tool to be used by EC, TA authorities and possibly by OEMs
- Close collaboration between DG-CLIMA, JRC and ACEA
- Major markets outside Europe already adopted initiatives (mainly simulation based)



Approach Chosen: Simulation

- Approaches explored :
 - *measurement on chassis dynamometer*
 - *measurement with PEMS*
 - *vehicle simulation*

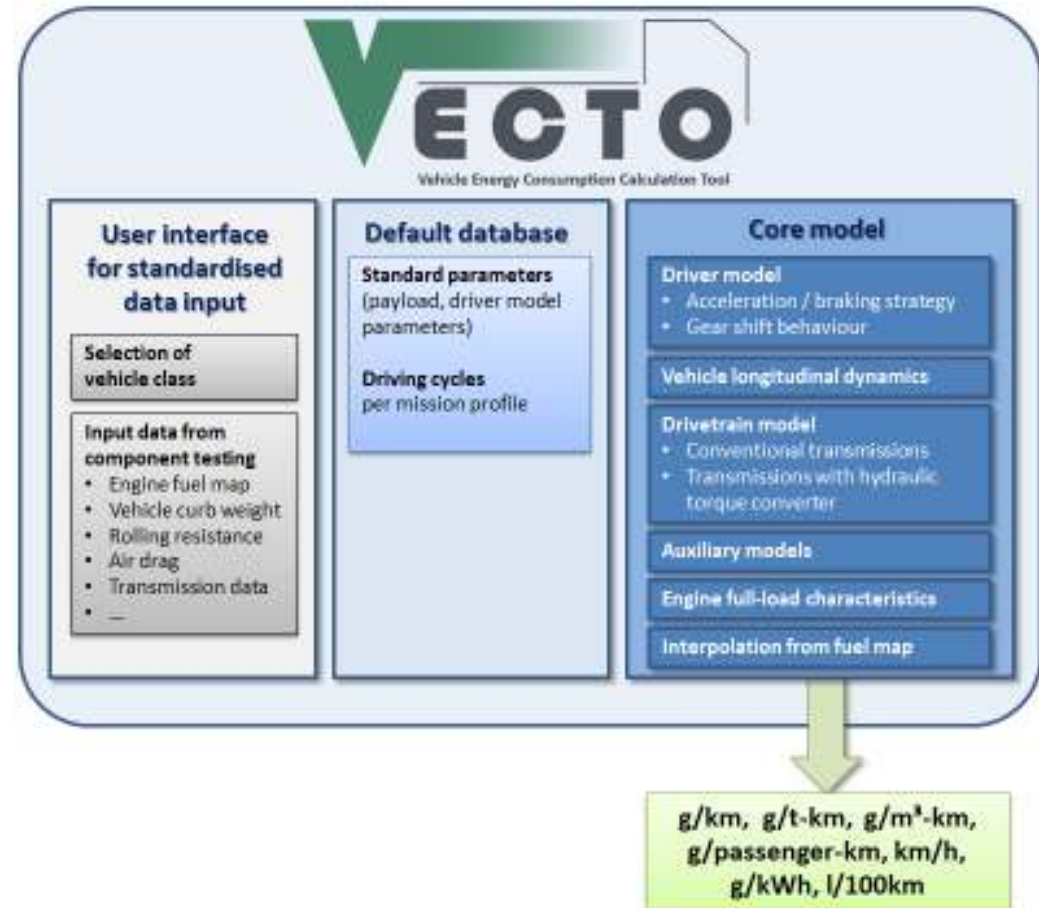
- Selected option:



- *Model based simulation for the whole vehicle (truck and trailer) and component testing*
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- Methodology considers:
 - *engine, driving resistances of whole vehicle (rolling, aerodynamic), gearbox, axles, most relevant auxiliaries, driver model, specific mission profiles-cycles*

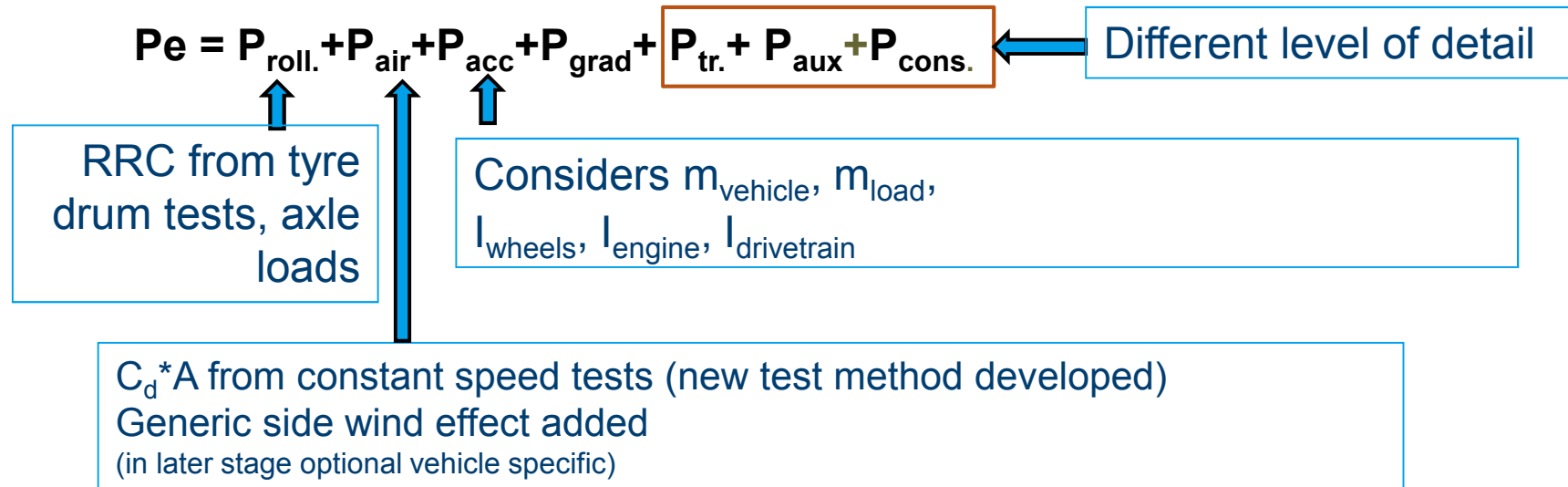
VECTO: The CO₂ simulation tool for HDVs in Europe

- **Vehicle Energy Consumption calculation TOol**
- Initially to cover:
 - **Delivery trucks (long haul and regional-city)**
 - **Coaches**
 - **Effort to include city buses**
- Effort to standardize:
 - **Measurement protocols for input data generation**
 - **Individual component simulation models**
 - **Mission profiles and cycles**
 - **Evaluation / validation approaches**



VECTO & INPUTS

Overview of simulator



Simulator (Vehicle Energy consumption Calculation Tool – VECTO):

- Backward simulation; Forward control loops included for target speed cycles, driver model operation, look ahead breaking, eco-roll, over-speeding
- Programming language: Visual Basic .NET
- Simulation of engine power and engine speed
- Interpolation of fuel consumption from engine map



Classification

- Total HDV classes:
 - 18 truck classes
 - 6 bus and coach classes
- 10 test cycles based on segment (5 for trucks and 5 for busses-coaches)
- Bodies and trailers:
 - Standard bodies and trailers
 - $\Delta(Cd \cdot A)$ measured for alternatives
- Simplifications being discussed

Axles	Identification of vehicle class				Segmentation (vehicle configuration and cycle allocation)					Norm-body allocation		
	Axle configuration	Chassis configuration	Maximum GVW [t]	vehicle class	Long haul	Regional delivery	Urban delivery	Municipal utility	Construction	Standard body	Standard trailer	Standard semitrailer
2	4x2	Rigid	>3.5 - 7.5	0		R	R			B0		
2	4x2	Rigid or Tractor	7.5 - 10	1		R	R			B1		
		Rigid or Tractor	>10 - 12	2	R	R	R			B2		
		Rigid or Tractor	>12 - 16	3		R	R			B3		
		Rigid	>16	4	R+T	R		R		B4	T1	
		Tractor	>16	5	T+S	T+S						S1
	4x4	Rigid	7.5 - 16	6				R	R	B1		
		Rigid	>16	7					R	B5		
Tractor		>16	8					T+S			W1?	
3	6x2/2-4	Rigid	all weights	9	R+T	R		R		B6	T2	
		Tractor	all weights	10	T+S	T+S						S2
	6x4	Rigid	all weights	11					R	B7		
		Tractor	all weights	12					R			S3
	6x6	Rigid	all weights	13					R	W7		
		Tractor	all weights	14					R	W7		
4	8x2	Rigid	all weights	15		R				B8		
	8x4	Rigid	all weights	16								
	8x6 & 8x8	Rigid	all weights	17								

R...Rigid,
T...Trailer,
T+S..Tractor+semi-trailer,
W...only weight

Steps:

Vehicle characteristics → Classification → Segmentation → Test cycle selection → vehicle loading and default / specific bodies allocation → simulation



Engine Module: VECTO relevant Input data (draft)

Component	Data	Unit	component specific	Default data	Comments	to be reported to TS	TS to be incorporated	CoP procedure
General	Vehicle class	[-]	X		classification according to HDV CO2 vehicle segmentation matrix			
	Vehicle curb weight	[kg]	X					
	Trailer or body curb weight	[kg]		X	specified for each vehicle class			
	Gross vehicle weight	[kg]	X					
	Axle load distribution	[%]		X	specified for each vehicle class			
	Chassis length	[m]	X		only for busses (→ number of passengers)			
	Chassis width	[m]	X		only for busses (→ number of passengers)			
Engine	Displacement	[ccm]	X					
	Rated power	[kW]	X					
	Idling speed	[rpm]	X					
	Rated speed	[rpm]	X					
	Engine rotational inertia incl. flywheel	[kgm ²]		X	calculated from engine displacement			
	Steady state fuel map	...	X		fuel consumption [g/h] = f (engine speed [rpm], engine torque [Nm])			
	Full-load curve	...	X		full-load torque = f (engine speed [rpm])			
	Drag curve	...	X		drag torque = f (engine speed [rpm])			
Test result WHTC hot	...	X		fuel consumption [g/h] = f (engine speed [rpm], engine torque [Nm]) in 10Hz time resolution				



Engine Module: general provisions (draft phase)

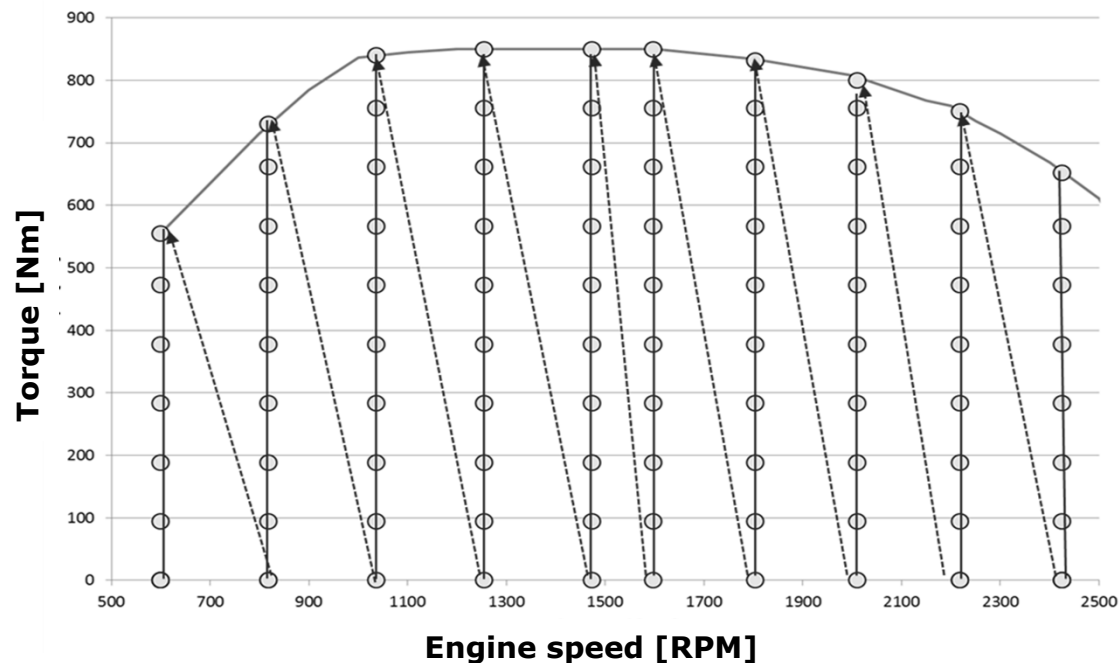
- Fuel consumption map → actual engine fuel consumption measured over different steady state conditions
- For each engine hardware and ECU calibration software combination a fuel map has to be measured
- All measurements performed according to (EC) 595/2009 on type approval of motor vehicles and engines and UN/ECE Regulation No 49.06
- Power consumption of engine auxiliaries (eg oil pump, coolant pump, fuel delivery pump, high pressure pump, alternator) to be covered by the map
- Issues that may arise because of the steady state approach:
 - Possible inconsistencies between engine certified CO₂ (WHTC hot part) and the steady state fuel map
 - transient engine behaviour not considered
- Solution → use of “WHTC correction factor” calculated on the basis of the actual WHTC measurement





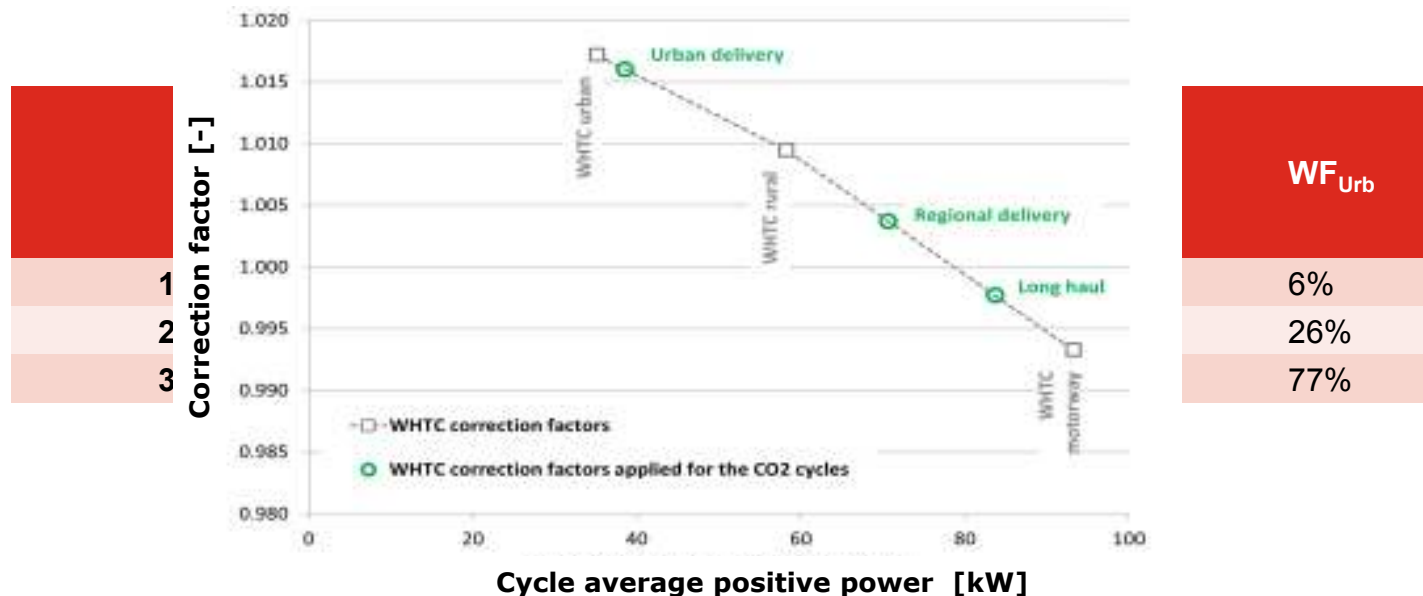
Engine Module: The engine map

- Minimum 10 engine speeds shall be measured. The four base speeds shall be: n_{idle} , $n_{pref} - n_{pref} * 0.04$, $n_{pref} + n_{pref} * 0.04$, n_{95}
- The remaining 6 engine speeds determined by splitting the two ranges (n_{idle} to $n_{pref} - 4\%$ and $n_{pref} + 4\%$ to n_{95}) into a minimum of 4 equidistant sections
- Torque step width: clustering range 0 - maximum torque into 10 equidistant sections
- Fill up the range below the mapping curve.
- When exceeding mapping curve the full load torque becomes applicable.



Engine Module: WHTC correction factors (draft)

- Engine only operation is simulated over the 3 parts of WHTC
 - fuel consumption calculated from the steady state fuel map (“backward calculation”)
- Measured specific FC per part in [g/kWh] is then divided by the simulated value
 - 3 different correction factors (CFs) calculated
- Total factor (CF_{Tot-i}) weighted average depending on mission profile “i”
 - Produced by VECTO by mission profile specific weighting factors (WFi),
 - $CF_{Tot-i} = CF_{Urb} \times WF_{Urb-i} + CF_{Rur} \times WF_{Rur-i} + CF_{MW} \times WF_{FMW-i}$

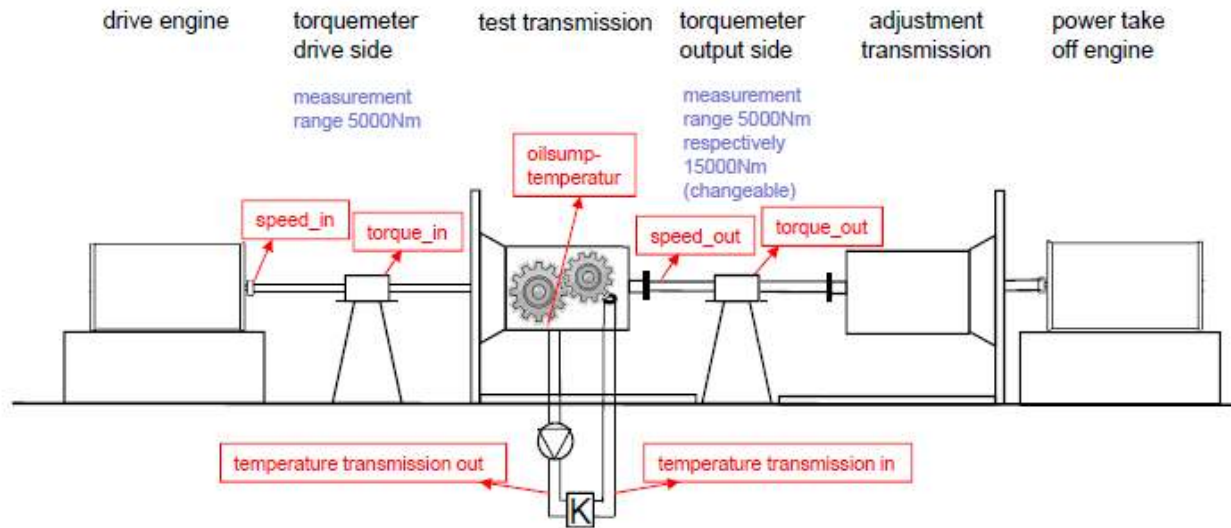


Transmission: VECTO relevant Input data (draft)

Component	Data	Unit	component specific	Default data	Comments	to be reported to TS	TS to be incorporated	CoP procedure
	Tyre rotational inertia			X	calculated based on wheel dimension of each axle			
	Tyre RRC (trailer)			X	if applicable			
	Tyre rotational inertia (trailer)			X	if applicable			
Transmission	Transmission type	[-]	X		Manual transmission (MT), Automated manual transmission (AMT) or Automatic Transmission with Torque converter (AT)			
	Torque loss map (mechanical)	...	X	X	for each gear: torque loss [Nm] = f (clutch output speed [rpm], clutch output torque [Nm])			
	Gear ratio	[-]	X		for each gear			
	Torque converter (TC) characteristics	...	X	X(?)	if applicable: torque ratio [-] = f (TC speed ratio [-]) reference torque at reference speed [Nm] = f (TC speed ratio [-])			
	Torque converter reference speed	[rpm]	X		if applicable; (1000 rpm defined as standard?)			
	Gearbox inertia	[kgm ²]		X	for transmissions w/o TC set to zero; transmissions with TC: open			
Retarder	Retarder type	[-]	X		none (or transmission internal) / primary / secondary			
	Retarder losses	...	X	X	if applicable: retarder losses [Nm] = f (retarder speed [rpm])			

Transmission: general provisions (draft)

- 3 different methods for assessing transmission losses
 - Option 1: Fall back values based on the maximum rated torque of the transmission
 - Option 2: Torque independent losses (measured), torque dependent losses (calculated). Electric machine & torque sensor before transmission (output shaft free-rotating)
 - Option 3: Measurement of total torque loss. Electric machines and torque sensors in front and behind transmission



- test transmission (may be rolled in)
- transmission installation position: horizontal
- torque accuracy: state of the art; measurement frequency at least 100Hz
- measuring point should be maintained as exactly as possible.
- the measuring temperature should be maintained in a range of $\pm 3K$. e.g.: $80^{\circ}C \pm 3K$
- oil filling similar to current production configuration (up to oil filler hole lower rim)

Source: ACEA



Transmission: Option 1 Fall back values

- Fall back values based on the maximum rated torque of the transmission
- The torque loss $T_{l,in}$ on the input shaft of the transmission is calculated:

$$T_{l,in} = T_{d0} + T_{d1000} \cdot \frac{n_{in}}{1000 \text{ rpm}} + f_T \cdot T_{in}$$

Where $T_{l,in}$ torque losses at input shaft

T_{dx} drag torque at x RPM

n_{in} speed of input shaft

f_t equals 1-efficiency (fixed depending on direct / non direct gear)

T_{in} torque at input shaft

$$\rightarrow T_{dx}(T_{max}) = T_{d0} = T_{d1000} = T_{const} \cdot \frac{T_{max \text{ in}}}{2000 \text{ Nm}}$$



Transmission: Option 2 (mix measured and calculated)

- Torque independent losses (measured),
- Torque dependent losses (calculated)
- Electric machine and torque sensor in front of transmission (output shaft free rotating)
- The torque loss $T_{l,in}$ on the input shaft of the transmission is:

$$T_{l,in}(n_{in}, T_{in}, gear) = T_{idle}(n_{in}, gear) + (1 - \eta_T(gear)) \cdot T_{in}$$

- $T_{idle} \rightarrow$ Drag torque from testing at 0 load [Nm] (measured component)
- Gear dependent efficiency $\eta_T \rightarrow$ calculated for each gear separately (calculated component)

$$\eta_T = \eta_{m,splitter} \cdot \eta_{m,main} \cdot \eta_{lowrange} \cdot \eta_{bearings}$$

- Fixed values or specific formulas for subcomponents





Transmission: Option 3 (full measurement)

- Measurement of total torque loss
- Electric machines and torque sensors at both sides of transmission
- General model as in option 2

$$T_{l,in}(n_{in}, T_{in}, gear) = T_{idle}(n_{in}, gear) + (1 - \eta_T(gear)) \cdot T_{in}$$

- The torque loss measured for (speed of the input shaft):
 - 600, 800, 1000, 1200, 1400, 1700, 2000, 2400, 2800, 3200, ... rpm up to the maximum speed according to the specifications of the transmission (or higher).
- At each speed, torque measured for (input torques):
 - 0, 200, 400, 600, 800, 1000, 1200, 1400, 1700, 2000, 2400, 2800, 3200, 3600, 4000, ... Nm up to the maximum input torque according to the specifications of the transmission (or higher)





Retarder: general provisions (draft phase)

- 2 different methods for assessing retarder losses
 - Option 1: standard technology specific table value for drag torque losses
 - Option 2: measurement of drag torque in deactivated mode

- Option 1:

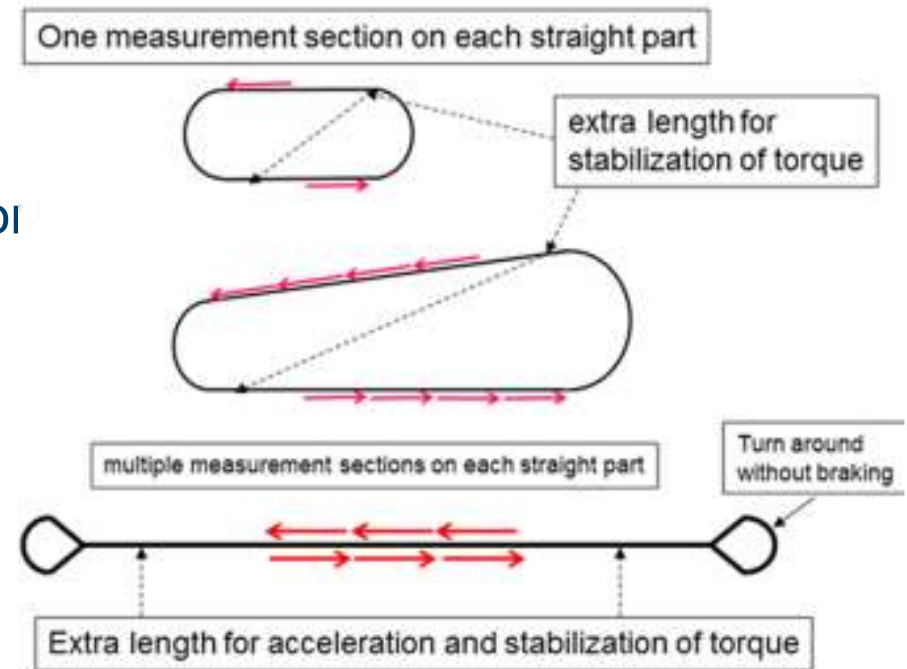
$$T_{1,Ret, input / prop} = 10 + 2 \cdot \left(\frac{n_{input / prop}}{1000} \right)^2$$

- Option 2:
- Retarder losses measured in combination with transmission testing
→ The transmission losses already include the retarder losses.
- If retarder individual component, retarder losses determined by subtracting gearbox losses measured with and without the retarder over one gear ratio



Input: Aerodynamic drag - rrc

- Constant speed test (at 2 velocities)
 - torque meter rim
 - anemometer
 - correction for gradient and for vehicle speed variations
 - correction for ambient p, T
 - $F = F_0 + C_d * A * v^2 * \rho / 2$



Important tire and vehicle conditioning for accurate $C_d * A$ results.

RRC calculated in these tests not to be used. Official value to be used for monitoring purposes

Gearshift model

- Implementation of gear shift strategy proposed by ACEA for manual and automated manual transmissions

Up- and down-shift polygons

Torque [Nm]	Downshift [rpm]	Upshift [rpm]
-500	650	900
0	650	900
500	700	950
...

Default-Option: skipping of gears: Criteria:

- 1) rpm is still over DownShift-rpm and
- 2) torque reserve is above a user-defined value (e.g. 20%)

Additional parameter for avoidance of oscillating shifts:

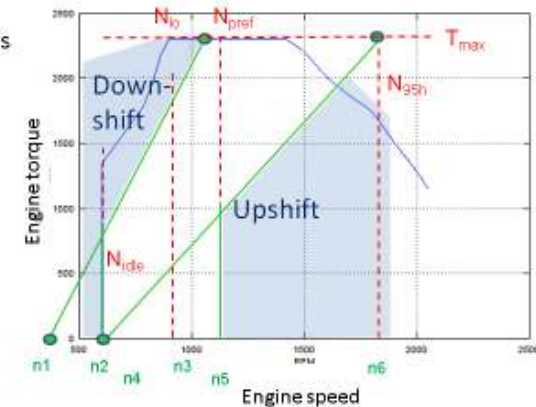
minimum time between two gear shifts (e.g. 3s)

- AMT = MT with different polygons and early upshifting
- Skipping gears possible based on torque reserve criteria, starting from gear > 1
- Automatic GB model under development based on input received from OEMs and GB manufacturers

Generic shift conditions (manual gearbox)

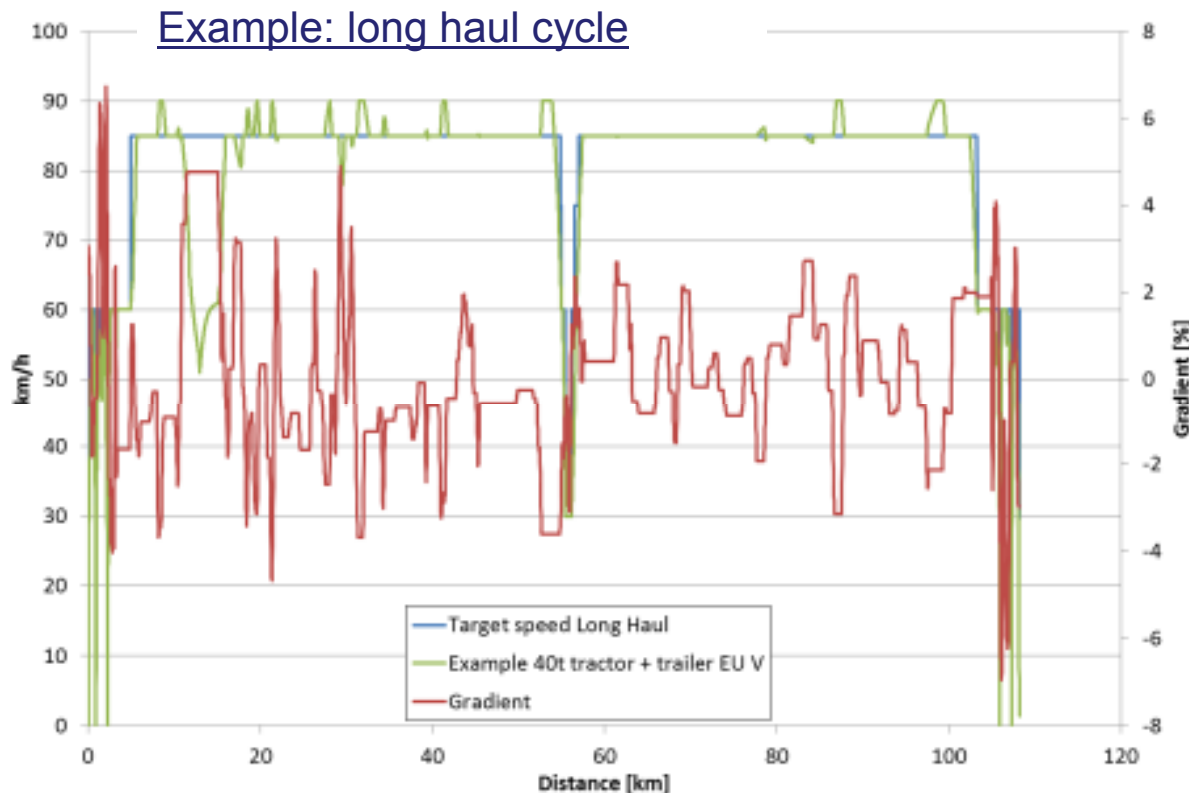
Proposal:

- $n1 \leftarrow N_{idle} / 2$
- $n2 \leftarrow N_{idle}$
- $n3 \leftarrow (N_{io} + N_{pref}) / 2$
- $n4 \leftarrow N_{idle}$
- $n5 \leftarrow N_{pref}$
- $n6 \leftarrow N_{gsh}$



Input: Test cycles - driver model

→ Different representative cycles per vehicle category and mission profile including target speed phases and road gradients



Driver model:

Acceleration: limited by full load and max. driver demand

Gear selection with torque interruption

Overspeed function optional eco-roll or none

“Look ahead” braking

Cycles: Trucks: Long haul, Regional delivery, urban delivery, Municipal utility, Construction
Busses: Urban bus (heavy urban, urban, suburban), Interurban bus, Coach





General structure of auxiliary models

Additional load to ICE from auxiliary operation
 „ $P_{mech,ICE}$ “ calculated in VECTO in 1Hz

$$P_{mech,ICE} = \frac{1}{\eta_{trans}} \cdot f \left(n_{ice} \cdot i_{aux}, \frac{P_{sup}}{\eta_{sup}} \right)$$

„performance map“

Alternator Average electric power demand

Compressor Average compressor supply power (Integral volume-flow

Steering pump Steering power course over distance ($M_{wheel} * \omega$) [kW]

Air conditioning e.g. cooling capacity (mass flow * ($h_{out} - h_{in}$)) [kW]

Auxiliary speed [rpm]	Supply power [kW]	Mechanical power [kW]
1415	0	0.07
1415	0.53	0.87
1415	0.64	1.03
1415	0.75	1.17
1416	0.84	1.36
1416	1.4	2.4
1887	0	0.07
...

Engine cooling system: special case

Detailed air-conditioning and air pump sub-models to developed by ACEA

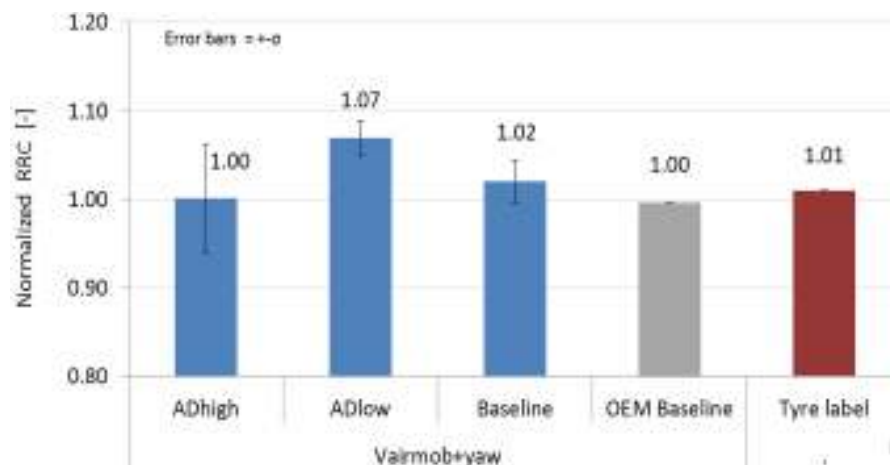
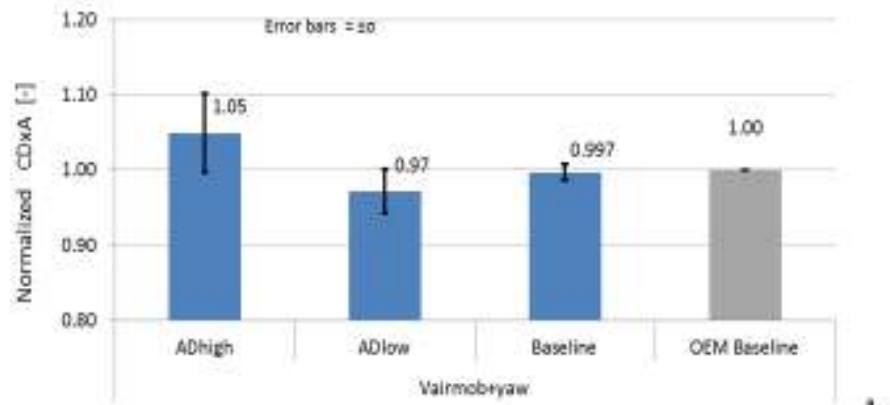
Operation profiles and/or generic default values for auxiliaries-vehicle-mission profile combinations are under investigations



VALIDATION SUMMARY

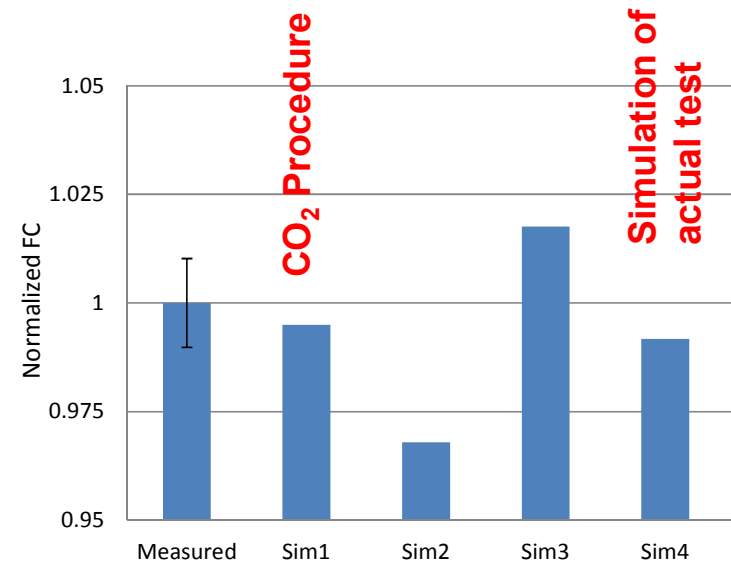
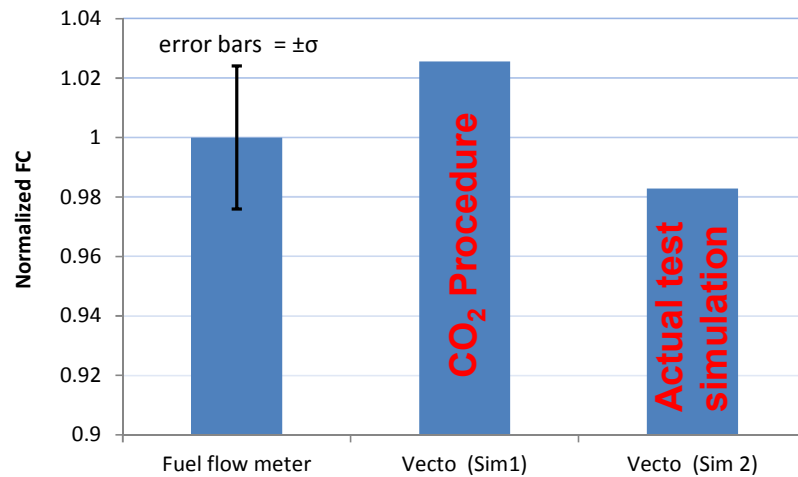
Results Air Drag With Yaw correction

- Application of generic yaw correction curve improves accuracy (>99%)
- Very good reproducibility in a different proving ground



Difference from OEM measurement for $C_d \cdot A_{cr}$ [%]	- 0.3 %
Standard deviation of $C_d \cdot A_{cr}$ measurement [%]	1.1 %
Difference from OEM value for RRC [%]	2.0 %
Standard deviation of RRC measurement [%]	2.3 %

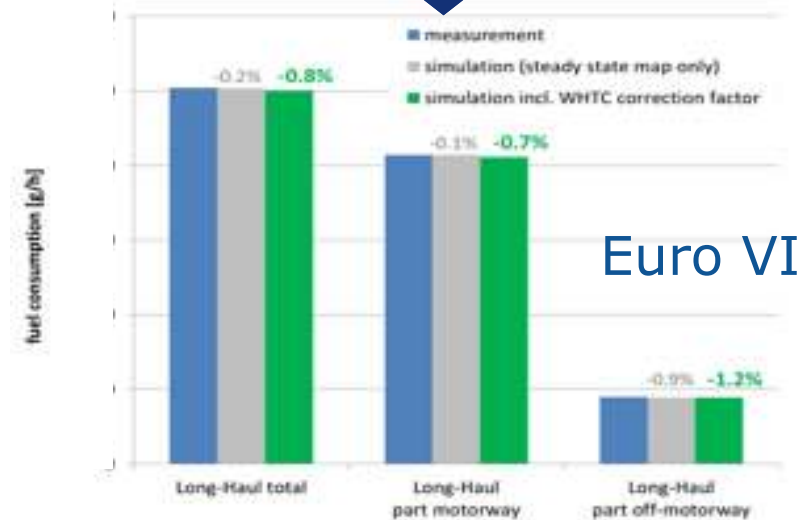
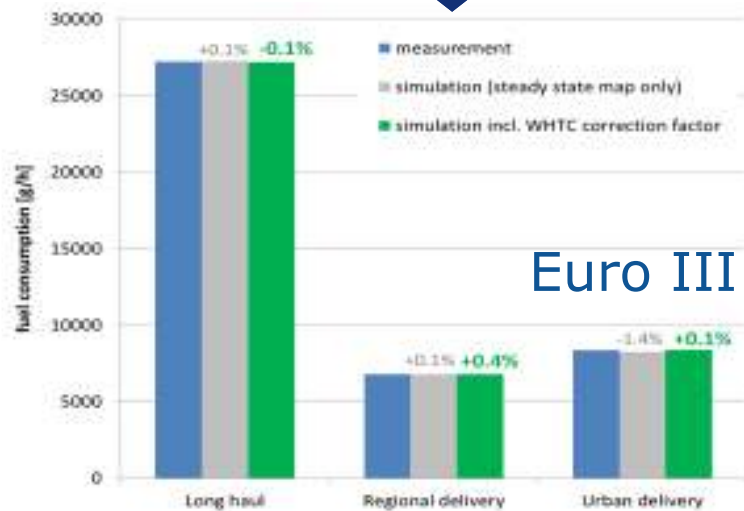
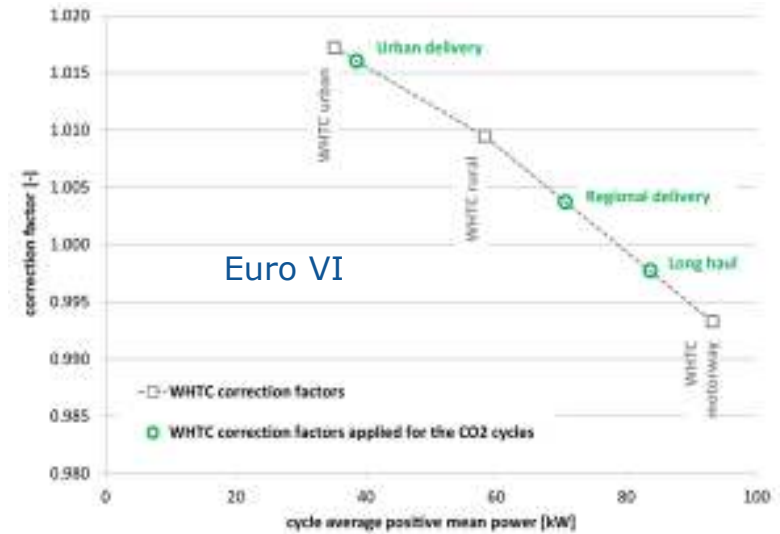
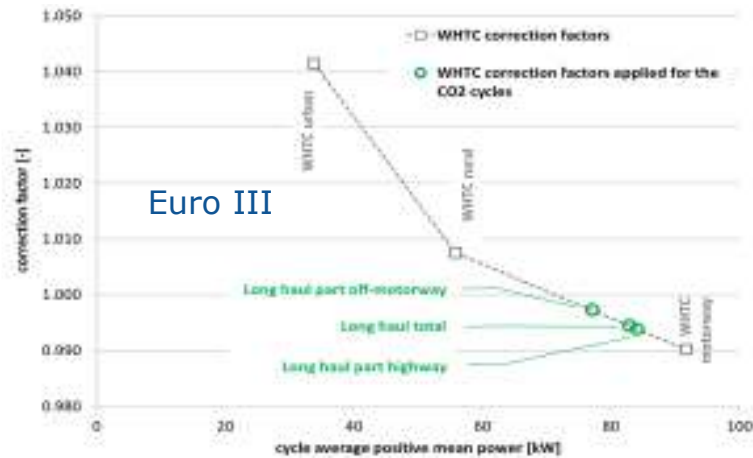
On road testing: summary of results



Method seems to be quite accurate, even before full development (results are even better than expected but this may be by chance)

On-going: Extensive experimental campaign to verify overall performance with several different kinds of vehicles.

Engine mapping



CONCLUSIONS & FOLLOW UP



Conclusions

- The declaration method (DM) proposed can provide results representative of the real world performance
- Accurate input data essential, positive feedback regarding the quality of developing measurement methods
- Simulator presents satisfactory accuracy within a $\pm \sim 3\%$ from measurements
- Good results from engine mapping approach & other modeling concepts introduced





Follow up

- Finalize & validate topics remaining open (*gearbox and driveline efficiency quantification, auxiliary units power consumption, automatic gear shifting strategies, mobile air conditioning simulation for city buses*)
- Accurate quantification of uncertainties for different vehicle types
- Apply the method to additional vehicle types / components, generate data. Lay down the foundations for a full scale application on different vehicles (pilot phase)
- Shift to forward simulation tool, attempt to merge with HILs simulator used for Hybrid HD powertrains



Thank you for your attention

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